

## Solution TD N°2

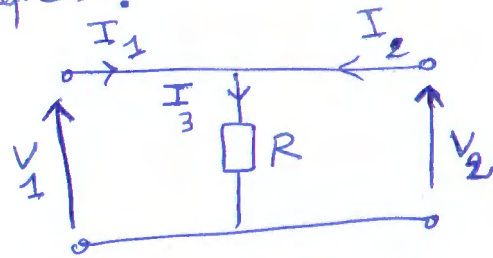
## Électromagnétique fondamentale I

## Exercice N°1:

\* La matrice impédance  $[Z]$  du quadripôle  $Q'$ :

on a deux équations caractéristiques:

$$\begin{cases} I_1 + I_2 = I_3 = V_1/R & \text{--- (1)} \\ V_1 = V_2 & \text{--- (2)} \end{cases}$$



de (1) :  $V_1 = R(I_1 + I_2)$

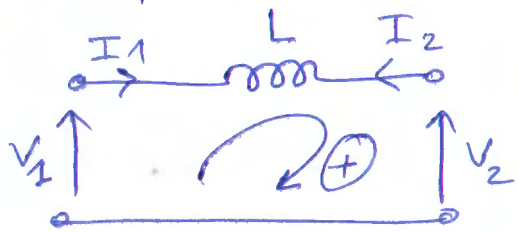
et  $V_1 = V_2 = R(I_1 + I_2)$  donc :

$$\begin{cases} V_1 = R I_1 + R I_2 \\ V_2 = R I_1 + R I_2 \end{cases}$$

sous forme matricielle on a:  $\begin{pmatrix} V_1 \\ V_2 \end{pmatrix} = \begin{pmatrix} R & R \\ R & R \end{pmatrix} \begin{pmatrix} I_1 \\ I_2 \end{pmatrix}$

\* La matrice  $[Y]$  du Quadripôle  $Q''$ :

$$\begin{cases} I_1 = -I_2 & \text{--- (1)} \\ V_1 - jL\omega I_1 - V_2 = 0 & \text{--- (2)} \end{cases}$$



de (2) :  $I_1 = \frac{V_1 - V_2}{jL\omega}$  donc

$$\begin{cases} I_1 = \frac{1}{jL\omega} V_1 - \frac{1}{jL\omega} V_2 \\ I_2 = -\frac{1}{jL\omega} V_1 + \frac{1}{jL\omega} V_2 \end{cases}$$

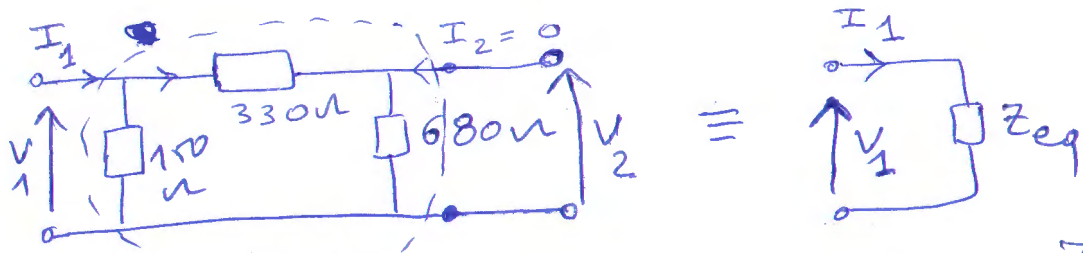
sous forme matricielle :  $[Y] = \begin{pmatrix} \frac{1}{jL\omega} & -\frac{1}{jL\omega} \\ -\frac{1}{jL\omega} & \frac{1}{jL\omega} \end{pmatrix}$

## Exercice N°2:

1°) La matrice  $[Z]$  :

$$Z_{11} = \frac{V_1}{I_1} \Big|_{I_2=0}$$

$$\text{et } Z_{21} = \frac{V_2}{I_1} \Big|_{I_2=0}$$



on a :  $V_1 = Z_{eq} I_1$  avec :  $Z_{eq} = (330 + 680) \parallel 150$

$$\Rightarrow Z_{eq} = \frac{1010 \cdot 150}{1010 + 150} = 130,6 \Omega$$

donc :  $Z_{eq} = \frac{V_1}{I_1} = Z_{11} = 130,6 \Omega$

\*  $Z_{21} = \frac{V_2}{I_1} \Big|_{I_2=0}$  ; D'après le diviseur de tension :

$$V_2 = \frac{680 V_1}{680 + 330} \text{ avec : } V_1 = Z_{eq} I_1 = Z_{11} I_1$$

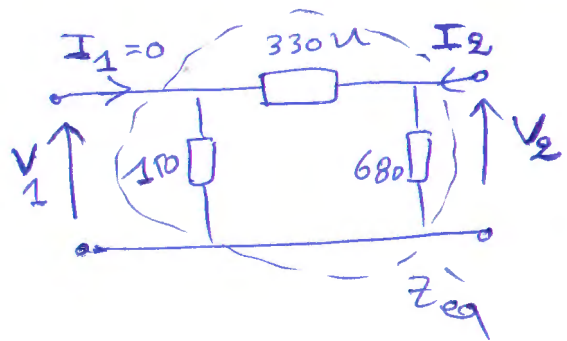
$$\Rightarrow V_2 = \frac{680 \cdot Z_{11} I_1}{1010} \Rightarrow \frac{V_2}{I_1} = \frac{680 \cdot Z_{11}}{1010}$$

$$\Rightarrow \boxed{Z_{21} = 87,9 \Omega}$$

avec :  $Z_{12} = Z_{21} = 87,9 \Omega$  (propriété de ~~reciprocite~~ réciprocity)

\*  $Z_{22} = \frac{V_2}{I_2} \Big|_{I_1=0}$

$$Z'_{eq} = (150 + 330) \parallel 680 = \frac{480 \cdot 680}{480 + 680} = 281,37 \Omega$$



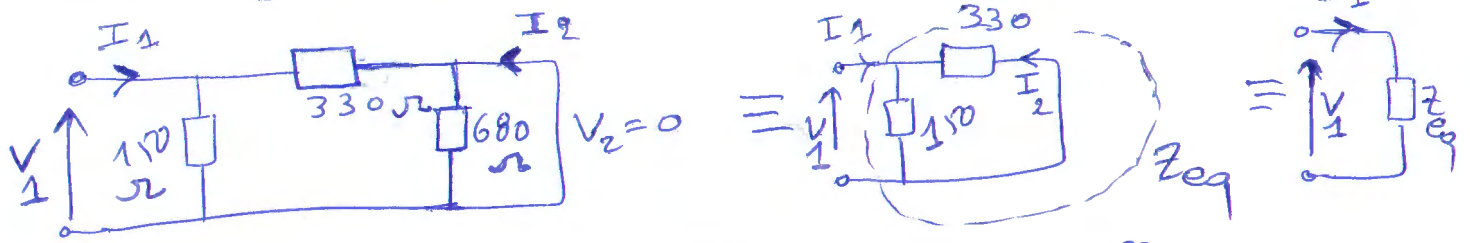
on a :  $V_2 = Z'_{eq} I_2 \Rightarrow Z_{22} = \frac{V_2}{I_2} = 281,37 \Omega$

$$[Z] = \begin{pmatrix} 130,6 & 87,9 \\ 87,9 & 281,37 \end{pmatrix}$$

2°/ la matrice  $[Y]$  :

\* Méthode 1 :

$$Y_{11} = \frac{I_1}{V_1} \Big|_{V_2=0} \quad ; \quad Y_{21} = \frac{I_2}{V_1} \Big|_{V_2=0}$$



avec:  $Z_{eq} = \frac{330 \cdot 150}{330 + 150} = \frac{330 \cdot 150}{330 + 150} = 103,12 \Omega$

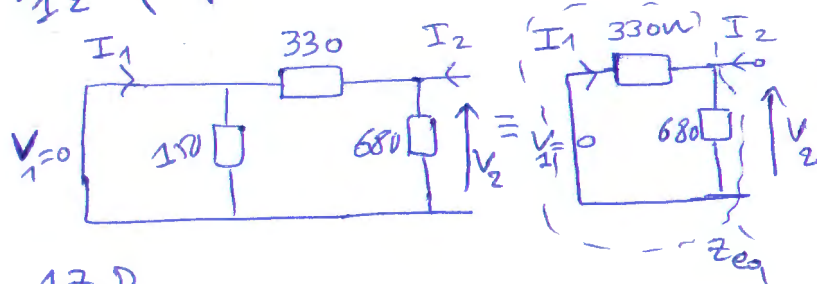
on a:  $V_1 = Z_{eq} I_1 \Rightarrow Y_{11} = \frac{I_1}{V_1} = \frac{1}{Z_{eq}} = 9,6 \cdot 10^{-3}$

$Y_{21} = \frac{I_2}{V_1} \Big|_{V_2=0}$  ; on a:  $V_1 = -330 I_2 \Rightarrow$

$$\frac{I_2}{V_1} = -\frac{1}{330}$$

$\Rightarrow Y_{21} = -3,03 \cdot 10^{-3} = Y_{12}$  (propriété de réciprocité)

\*  $Y_{22} = \frac{I_2}{V_2} \Big|_{V_1=0}$



$Z'_{eq} = \frac{330 \cdot 680}{330 + 680} = 222,17 \Omega$

$V_2 = Z'_{eq} I_2 \Rightarrow Y_{22} = \frac{I_2}{V_2} = \frac{1}{Z'_{eq}} = \frac{1}{222,17} = 4,5 \cdot 10^{-3}$

$$[Y] = \begin{pmatrix} 9,69 \cdot 10^{-3} & -3,03 \cdot 10^{-3} \\ -3,03 \cdot 10^{-3} & 4,5 \cdot 10^{-3} \end{pmatrix}$$

\* 2<sup>ème</sup> méthode: on a:  $[Y] = [Z]^{-1} = \frac{1}{\det[Z]} \text{adj}[Z]$

$$\text{adj}[Z] = \begin{pmatrix} Z_{22} & -Z_{12} \\ -Z_{21} & Z_{11} \end{pmatrix}$$

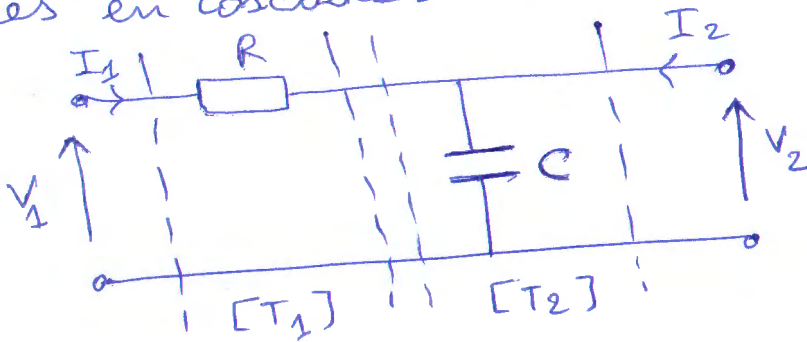
$$[Y] = \frac{1}{130,6 \cdot 281,37 - (87,9)^2} \begin{pmatrix} 281,37 & -87,9 \\ -87,9 & 130,6 \end{pmatrix}$$

$$= \begin{pmatrix} 9,69 \cdot 10^{-3} & -3,03 \cdot 10^{-3} \\ -3,03 \cdot 10^{-3} & 4,5 \cdot 10^{-3} \end{pmatrix}$$

Exercice N° 3 :

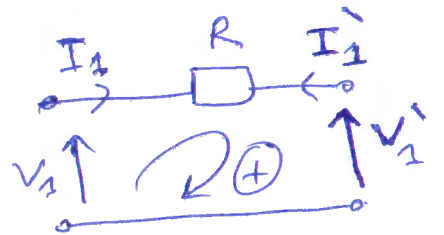
1°/ La matrice de transfert  $[T]$  :

on décompose le quadripôle en deux quadripôles associés en cascade :



on détermine  $[T_1]$  et  $[T_2]$  :

$$[T_1] \begin{cases} V_1 - R I_1 - V_1' = 0 \\ I_1 = -I_1' \end{cases}$$

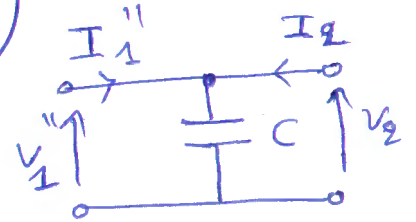


$$\begin{pmatrix} V_1' \\ I_1' \end{pmatrix} = [T_1] \begin{pmatrix} V_1 \\ -I_1 \end{pmatrix} \text{ donc : } \begin{cases} V_1' = V_1 - R I_1 \\ I_1' = 0 V_1 - I_1 \end{cases}$$

donc :  $[T_1] = \begin{pmatrix} 1 & R \\ 0 & 1 \end{pmatrix}$

$[T_2]$  ?

on a : 
$$\begin{cases} V_2 = V_1'' & \textcircled{1} \\ I_1'' + I_2 = \frac{V_1''}{\frac{1}{j\omega C}} & \textcircled{2} \end{cases}$$



de  $\textcircled{2}$  on a :  $I_2 = j\omega C V_1'' - I_1''$

$\Rightarrow [T_2] = \begin{pmatrix} 1 & 0 \\ j\omega C & 1 \end{pmatrix}$

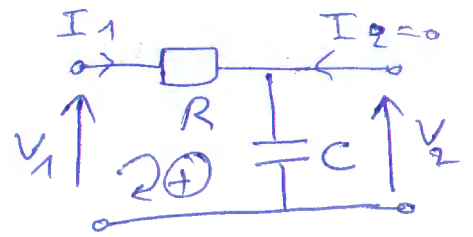
donc :  $[T] = [T_2] \cdot [T_1] = \begin{pmatrix} 1 & 0 \\ j\omega C & 1 \end{pmatrix} \cdot \begin{pmatrix} 1 & R \\ 0 & 1 \end{pmatrix} = \begin{pmatrix} 1 & R \\ j\omega C & 1+j\omega CR \end{pmatrix}$

2°/ La matrice  $[Z]$  du Q :

$Z_{11} = \frac{V_1}{I_1} \Big|_{I_2=0}$  ;  $Z_{21} = \frac{V_2}{I_1} \Big|_{I_2=0}$

Maille:  $V_1 - R I_1 - \frac{1}{j\omega C} I_1 = 0$

$\Rightarrow V_1 = \left( R + \frac{1}{j\omega C} \right) I_1$



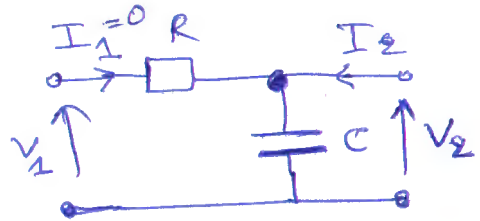
donc:  $Z_{11} = \frac{V_1}{I_1} = R + \frac{1}{j\omega C}$

$Z_{21} = \frac{V_2}{I_1}$ ? on a:  $V_2 = \frac{1}{j\omega C} I_1 \Rightarrow \frac{V_2}{I_1} = \frac{1}{j\omega C}$

$Z_{21} = \frac{1}{j\omega C} = Z_{12}$

\*  $Z_{22} = \frac{V_2}{I_2} \Big|_{I_1=0}$

$V_2 = \frac{1}{j\omega C} I_2$



$\Rightarrow \frac{V_2}{I_2} = \frac{1}{j\omega C} = Z_{22}$

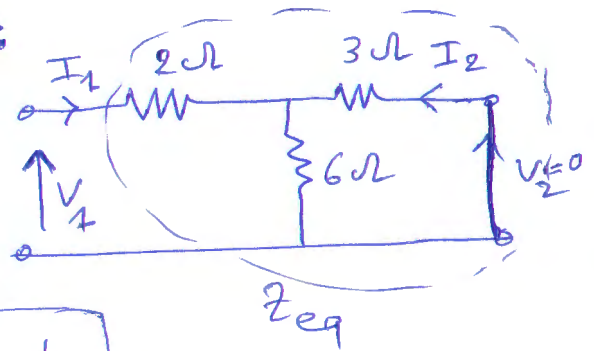
donc:  $[Z] = \begin{pmatrix} R + \frac{1}{j\omega C} & \frac{1}{j\omega C} \\ \frac{1}{j\omega C} & \frac{1}{j\omega C} \end{pmatrix}$

Exercice N°4:

La matrice hybride du  $\Phi$ :

on a:  $h_{11} = \frac{V_1}{I_1} \Big|_{V_2=0}$ ;  $h_{21} = \frac{I_2}{I_1} \Big|_{V_2=0}$

$Z_{eq} = (3 \parallel 6) + 2 = \frac{3 \cdot 6}{3+6} + 2 = 4$

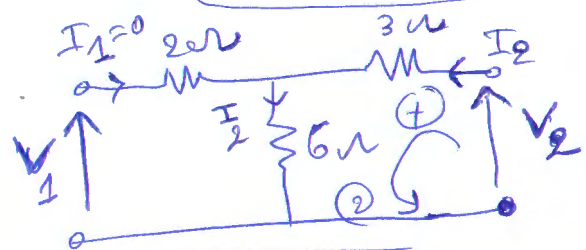


$V_1 = Z_{eq} I_1 \Rightarrow \frac{V_1}{I_1} = Z_{eq} = \boxed{h_{11} = 4}$

\*  $h_{21}$ ? on applique le diviseur de courant:

$I_2 = \frac{-6 I_1}{6+3} = -\frac{2}{3} I_1 \Rightarrow \boxed{h_{21} = -\frac{2}{3}}$

\*  $h_{22} = \frac{I_2}{V_2} \Big|_{I_1=0}$



Maille ②:  $V_2 - 3 I_2 - 6 I_2 = 0$

$\Rightarrow V_2 = 9 I_2 \Rightarrow \frac{V_2}{I_2} = \boxed{\frac{1}{9} = h_{22}}$

Le diviseur de tension :

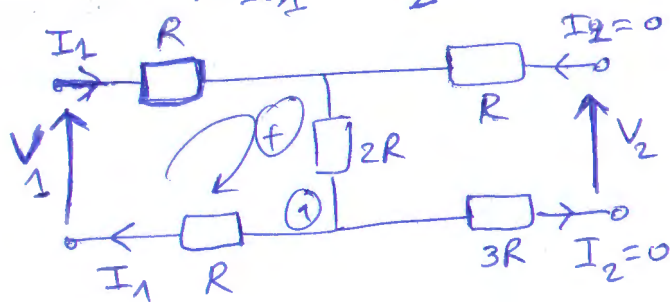
$$V_1 = \frac{6 \cdot V_2}{6 + 3} = \frac{2}{3} V_2 \Rightarrow h_{12} = \frac{V_1}{V_2} = \frac{2}{3}$$

$$\Rightarrow [h] = \begin{pmatrix} 4 & \frac{2}{3} \\ -\frac{2}{3} & \frac{1}{3} \end{pmatrix}$$

Exercice N° 5 :

\*  $[Z]$  du quadripôle  $Q_1$  :

$$Z_{11} = \frac{V_1}{I_1} \Big|_{I_2=0} ; Z_{21} = \frac{V_2}{I_1} \Big|_{I_2=0}$$



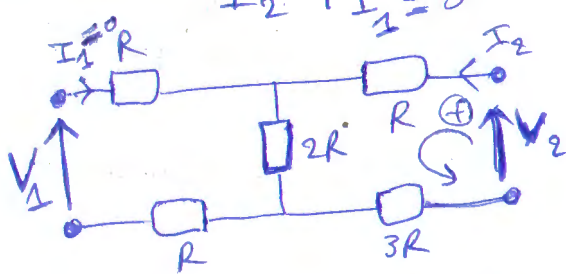
Maille ① :  $V_1 - R I_1 - 2R I_1 = R I_1$

$$\Rightarrow V_1 = 4R I_1$$

$$\Rightarrow Z_{11} = \frac{V_1}{I_1} = 4R$$

\*  $Z_{21}$  ? on a :  $V_2 = 2R I_1 \Rightarrow \frac{V_2}{I_1} = 2R = Z_{21}$

$$* Z_{22} = \frac{V_2}{I_2} \Big|_{I_1=0}$$



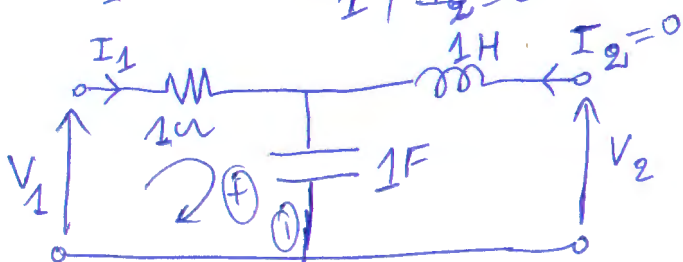
Maille 2 :  $V_2 - R I_2 - 2R I_2 - 3R I_2 = 0$

$$\Rightarrow V_2 = 6R I_2 \Rightarrow Z_{22} = 6R$$

donc :  $[Z] = \begin{pmatrix} 4R & 2R \\ 2R & 6R \end{pmatrix}$

\*  $[Z]$  du  $Q_2$  :

$$Z_{11} = \frac{V_1}{I_1} \Big|_{I_2=0} ; Z_{21} = \frac{V_2}{I_1} \Big|_{I_2=0}$$



Maille 1 :  $V_1 - I_1 - \frac{1}{j\omega} I_1 = 0$

$$\Rightarrow V_1 = \left(1 + \frac{1}{j\omega}\right) I_1$$

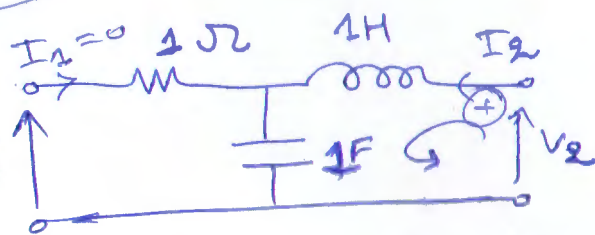
$$Z_{11} = \frac{V_1}{I_1} = 1 + \frac{1}{j\omega}$$

\*  $Z_{21}$  ? on a :  $V_2 = \frac{1}{j\omega} I_1 \Rightarrow Z_{21} = \frac{1}{j\omega}$

$$Z_{12} = \frac{1}{j\omega}$$

$$Z_{22} = \frac{V_2}{I_2} \Big|_{I_1=0}$$

$$\sum V_i = 0 \Rightarrow V_2 - j\omega I_2 - \frac{1}{j\omega} I_2 = 0$$



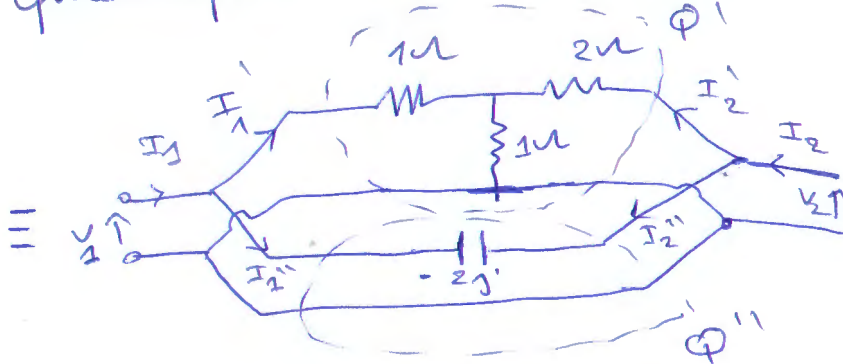
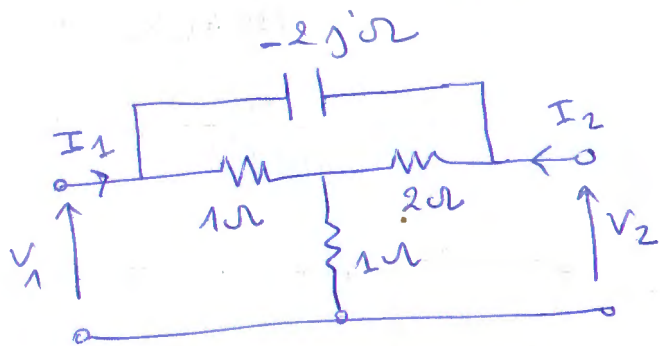
$$\Rightarrow V_2 = \left( j\omega + \frac{1}{j\omega} \right) I_2 = j \left( \omega - \frac{1}{\omega} \right) = j \left( \frac{\omega^2 - 1}{\omega} \right) I_2$$

donc :  $Z_{22} = j \left( \frac{\omega^2 - 1}{\omega} \right)$

$$[Z] = \begin{pmatrix} 1 + \frac{1}{j\omega} & \frac{1}{j\omega} \\ \frac{1}{j\omega} & j \left( \frac{\omega^2 - 1}{\omega} \right) \end{pmatrix}$$

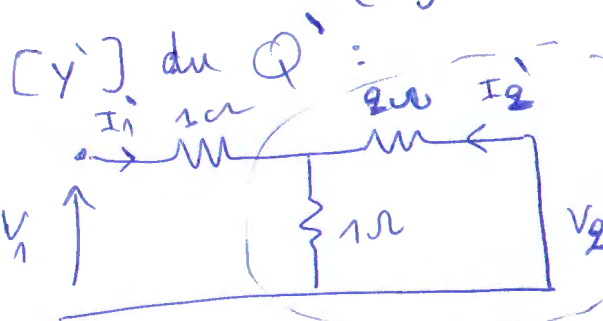
Exercice N°6 :

\* La matrice  $[Y]$  du quadripôle en T-ponté :



Le quadripôle  $Q'$  et  $Q''$  sont en // :

donc :  $[Y] = [Y'] + [Y'']$



$$Y'_{11} = \frac{I_1}{V_1} \Big|_{V_2=0}$$

on a :  $Z_{eq1} = 2 \parallel 1 = \frac{2 \cdot 1}{2+1} = \frac{2}{3} \Omega$

$$\Rightarrow Z_{eq} = Z_{eq1} + 1 = \frac{5}{3}$$

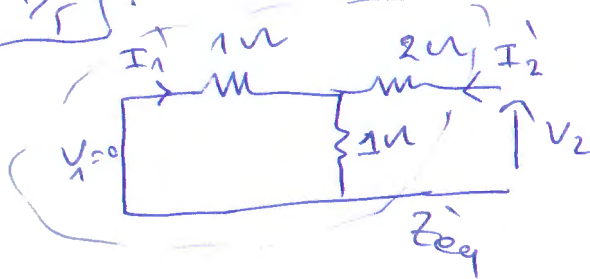
$$V_1 = Z_{eq} I_1 \Rightarrow \frac{I_1}{V_1} = \frac{1}{Z_{eq}} = \frac{3}{5}$$

$Y_{21}' = \frac{I_2'}{V_1} \Big|_{V_2=0}$  le diviseur de courant :

on a :  $I_2' = \frac{-1 \cdot I_1'}{1+2}$  et  $I_1' = Y_{11}' V_1$ .

donc :  $I_2' = \frac{-3/5 V_1}{1} \Rightarrow \frac{I_2'}{V_1} = -\frac{1}{5} = Y_{21}'$

$Y_{21}' = Y_{12}' = -\frac{1}{5}$



\*  $Y_{22}' = \frac{I_2'}{V_2} \Big|_{V_1=0}$

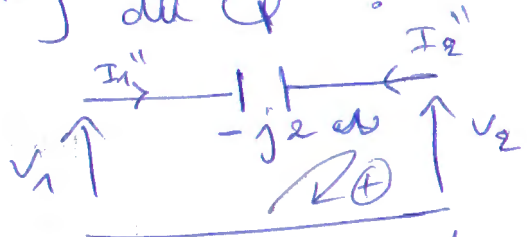
$Z_{eq} = 1 \parallel 1 \Omega + 2$

$= \frac{1 \cdot 1}{1+1} + 2 = \frac{1}{2} + 2 = \frac{5}{2}$

$V_2 = Z_{eq} I_2' \Rightarrow \frac{I_2'}{V_2} = 1/Z_{eq} = 2/5$

donc :  $[Y'] = \begin{pmatrix} 3/5 & -1/5 \\ -1/5 & 2/5 \end{pmatrix}$

\*  $[Y'']$  du  $Q''$  :



$V_1 + j\omega I_1'' - V_2 = 0$

$I_2'' = -I_1''$

$\Rightarrow \begin{cases} I_1'' = \frac{V_2 - V_1}{2j} \\ I_2'' = -I_1'' = \frac{V_1 - V_2}{2j} \end{cases} \Rightarrow \begin{cases} I_1'' = \frac{-1}{2j} V_1 + \frac{1}{2j} V_2 \\ I_2'' = \frac{1}{2j} V_1 - \frac{1}{2j} V_2 \end{cases}$

ou  $\begin{cases} I_1'' = j/2 V_1 - 1/2 j V_2 \\ I_2'' = -j/2 V_1 + 1/2 j V_2 \end{cases} \Rightarrow [Y''] = \begin{pmatrix} 1/2 j & -1/2 j \\ -1/2 j & 1/2 j \end{pmatrix}$

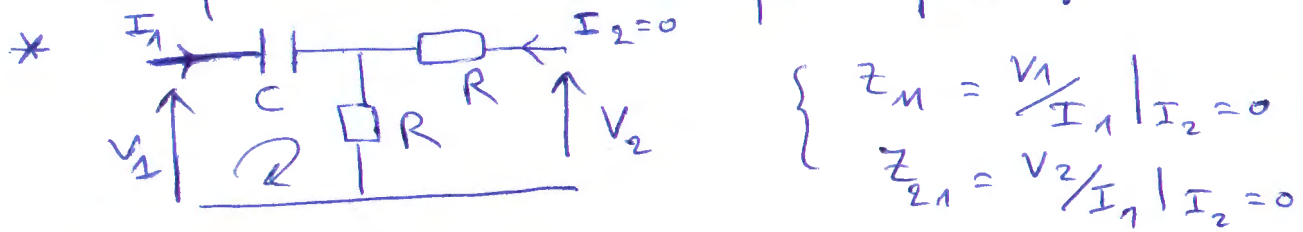
$[Y] = [Y'] + [Y''] \Rightarrow [Y] = \begin{pmatrix} 3/5 + 1/2 j & -1/5 + j/2 \\ -1/5 + j/2 & 2/5 + j/2 \end{pmatrix}$



## Exercice N° 7 :

1°/ L'impédance d'entrée :  $Z_e = \frac{V_1}{I_1} = Z_{11} - \frac{Z_{12} \cdot Z_{21}}{Z_{22} + Z_g}$

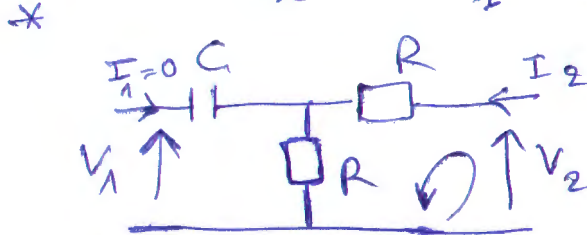
on doit calculer la matrice  $[Z]$  pour trouver l'impédance d'entrée du quadripôle :



on a :  $V_1 = (R + \frac{1}{j\omega C}) I_1 = 0$

$\Rightarrow \frac{V_1}{I_1} = R + \frac{1}{j\omega C} \Rightarrow Z_{11} = R + \frac{1}{j\omega C}$

et :  $V_2 = R I_1 \Rightarrow \frac{V_2}{I_1} = R \Rightarrow Z_{21} = Z_{12} = R$



$\sum V_i = 0 \Rightarrow V_2 - R I_2 - R I_2 = 0$   
 $\Rightarrow \frac{V_2}{I_2} = 2R \Rightarrow Z_{22} = 2R$

donc :  $Z_e = R + \frac{1}{j\omega C} - \frac{R \cdot R}{R + 2R} = \frac{1 + jRC\omega}{j\omega C} - \frac{R^2}{3R}$

$Z_e = \frac{3 + j^2 RC\omega}{j^3 \omega C}$

2°/ L'impédance de sortie :

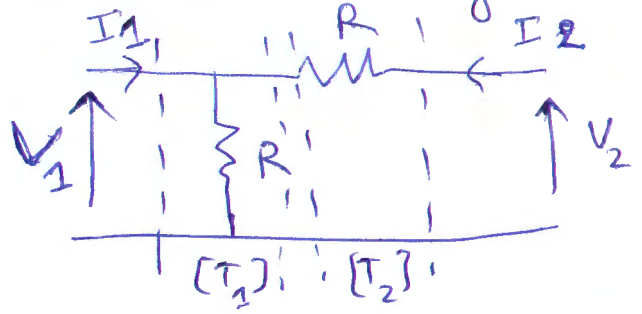
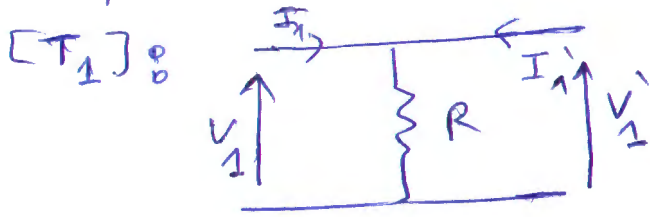
$Z_s = Z_{22} - \frac{Z_{12} \cdot Z_{21}}{Z_g + Z_{11}} \quad (Z_g = r)$

$Z_s = 2R - \frac{R \cdot R}{r + \frac{1 + jRC\omega}{j\omega C}} = 2R - \frac{R^2}{1 + j(R+r)C\omega}$

$Z_s = \frac{2R + j(R^2 + 2Rr)C\omega}{1 + j(R+r)C\omega}$

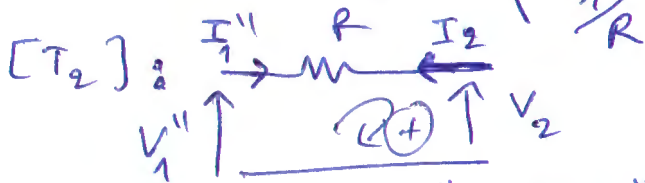
Exercice N° 8 :

Pour calculer le gain en tension et le gain en courant il faut calculer la matrice de transfert du quadripôle  $\mathcal{Q}$  :



$$\begin{cases} I_1 + I_1' = V_1 / R \\ V_1' = V_1 \end{cases} \Rightarrow \begin{cases} I_1' = \frac{1}{R} V_1 - I_1 \\ V_1' = V_1 \end{cases} \Rightarrow \begin{cases} V_1' = V_1 \\ I_1' = \frac{1}{R} V_1 - I_1 \end{cases}$$

$$\Rightarrow [T_1] = \begin{pmatrix} 1 & 0 \\ 1/R & 1 \end{pmatrix}$$



$$\begin{cases} V_1'' - R I_2'' - V_2 = 0 \\ I_2 = -I_1'' \end{cases}$$

$$\Rightarrow \begin{cases} V_2 = V_1'' - R I_1'' \\ I_2 = -I_1'' \end{cases}$$

$$\Rightarrow [T_2] = \begin{pmatrix} 1 & R \\ 0 & 1 \end{pmatrix}$$

$$[T] = [T_2] \cdot [T_1] = \begin{pmatrix} 2 & R \\ 1/R & 1 \end{pmatrix}$$

\* Le gain en tension :

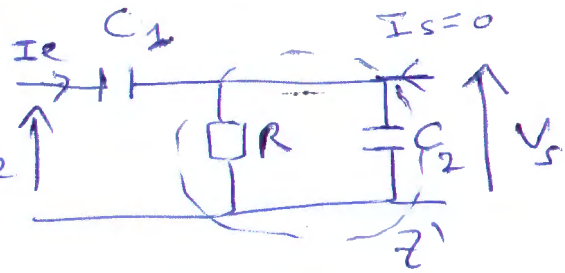
$$G_V = \frac{V_2}{V_1} = \frac{Z_u}{T_{22} Z_u + T_{12}} = \frac{R}{1 \cdot R + R} = \frac{1}{2}$$

\* Le gain en courant :

$$G_I = \frac{I_2}{I_1} = \frac{-1}{T_{11} + T_{21} Z_u} = \frac{-1}{2 + 1/R \cdot R} = -\frac{1}{3}$$

Exercice N°9

\* La fonction de transfert:  $V_s \uparrow$



$$H(j\omega) = \frac{V_s}{V_e} = \frac{Z'}{Z' + \frac{1}{j\omega C_1}}$$

avec:  $Z' = \frac{R \cdot \frac{1}{j\omega C_2}}{R + \frac{1}{j\omega C_2}} = \frac{R}{1 + j\omega R C_2}$

donc:  $H(j\omega) = \frac{R}{1 + j\omega R C_2} \times \frac{1}{\frac{1}{j\omega C_1} + \frac{R}{1 + j\omega R C_2}}$

$$= \frac{R}{1 + j\omega R C_2} \times \frac{1}{\frac{1 + j\omega R C_2 + j\omega R C_1}{j\omega C_1 (1 + j\omega R C_2)}}$$

$$= \frac{j\omega R C_1}{1 + j\omega R (C_1 + C_2)}$$

$$H(j\omega) = \frac{j\omega/\omega_1}{1 + j\omega/\omega_2}$$

avec:  $\omega_1 = \frac{1}{RC_1} = 1000 \text{ rad/s} = 10^3 \text{ rad/s}$

$\omega_2 = \frac{1}{R(C_1 + C_2)} = 100 \text{ rad/s}$

\* Le gain en dB:

$$G_{dB} = 20 \log_{10} |H(j\omega)| = 20 \log \frac{\omega}{\omega_1} - 20 \log \sqrt{1 + \left(\frac{\omega}{\omega_2}\right)^2}$$

$$= G_1 + G_2$$

\* La phase:  $\phi = \pi/2 - \arctg \frac{\omega}{\omega_2} = \phi_1 + \phi_2$

\* L'étude de  $\phi_1, G_1$ :

$$\begin{cases} G_1 = 20 \log \frac{\omega}{\omega_1} \rightarrow \text{c'est une droite de pente } 20 \frac{\text{dB}}{\text{dec}} \\ \phi_1 = \pi/2 \text{ rd} \rightarrow \text{droite horizontale.} \end{cases}$$

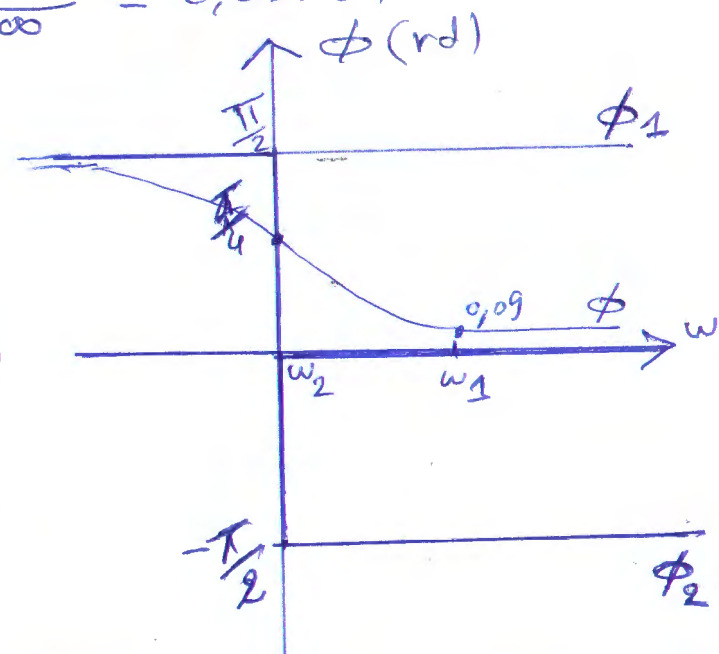
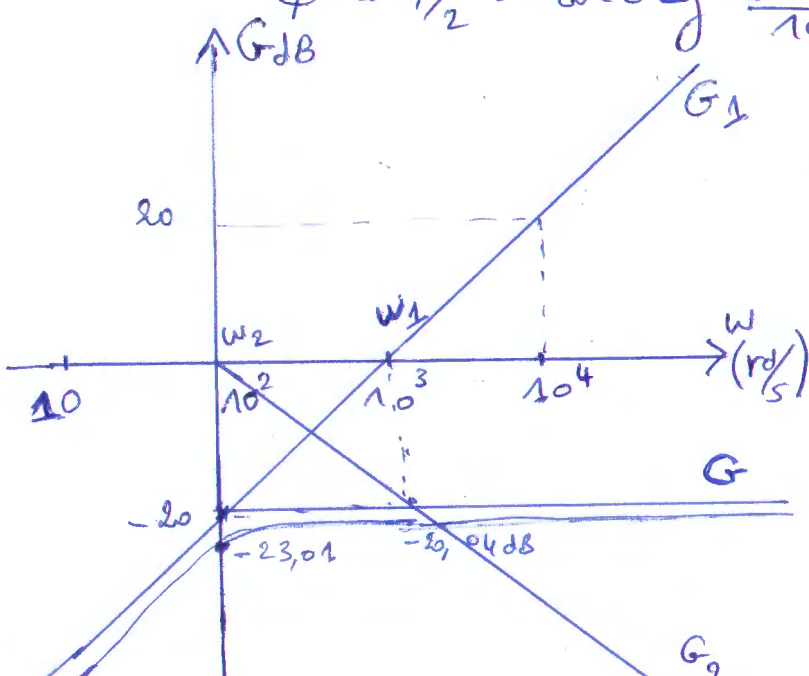
\* L'étude de  $G_2, \phi_2$ :

Les asymptotes :  $\omega \ll \omega_2 \begin{cases} G_2 = 0 \text{ dB} \\ \phi_2 = 0 \text{ rd} \end{cases}$

$\omega \gg \omega_2 \begin{cases} G_2 = -20 \log \frac{\omega}{\omega_2} \rightarrow \text{droite de pente } -20 \text{ dB/décad} \\ \phi_2 = -\pi/2 \text{ rd} \end{cases}$

Pour  $\omega = \omega_1 \Rightarrow G = 20 \log \frac{1000}{1000} - 20 \log \sqrt{1 + \left(\frac{1000}{100}\right)^2} = -20,04 \text{ dB}$

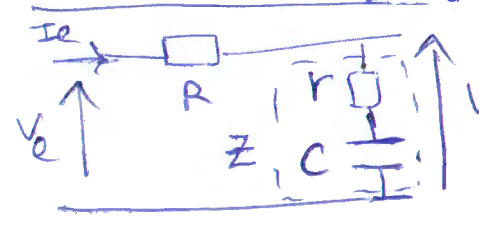
$\phi = \pi/2 - \arctg \frac{1000}{100} = 0,09 \text{ rd}$



c'est un filtre passe haut.

pour  $\omega = \omega_2 \begin{cases} \phi = \pi/4 \text{ rd} \\ G = -23,04 \text{ dB} \end{cases}$

Exercice N°10 : c'est un filtre à avance de  $r + \frac{1}{j\omega C} = \frac{z}{z + f}$



phase:  $H(j\omega) = \frac{V_s}{V_e} = \frac{z}{R + r + \frac{1}{j\omega C}} = \frac{z + f}{1 + j(R+r)C\omega}$

donc :  $H(j\omega) = \frac{1 + j\omega/\omega_1}{1 + j\omega/\omega_2}$

avec  $\omega_1 = \frac{1}{rc} = 10^4 \text{ rd/s}$ ;  $\omega_2 = \frac{1}{(R+r)C} = 10^3 \text{ rd/s}$

Le gain en dB :

$G_{dB} = 20 \log_{10} |H(j\omega)| = 20 \log_{10} \sqrt{1 + \left(\frac{\omega}{\omega_1}\right)^2} - 20 \log_{10} \sqrt{1 + \left(\frac{\omega}{\omega_2}\right)^2} = G_1 + G_2$

\* La phase :  $\phi = \text{arctg} \frac{\omega}{\omega_1} - \text{arctg} \frac{\omega}{\omega_2} = \phi_1 + \phi_2$

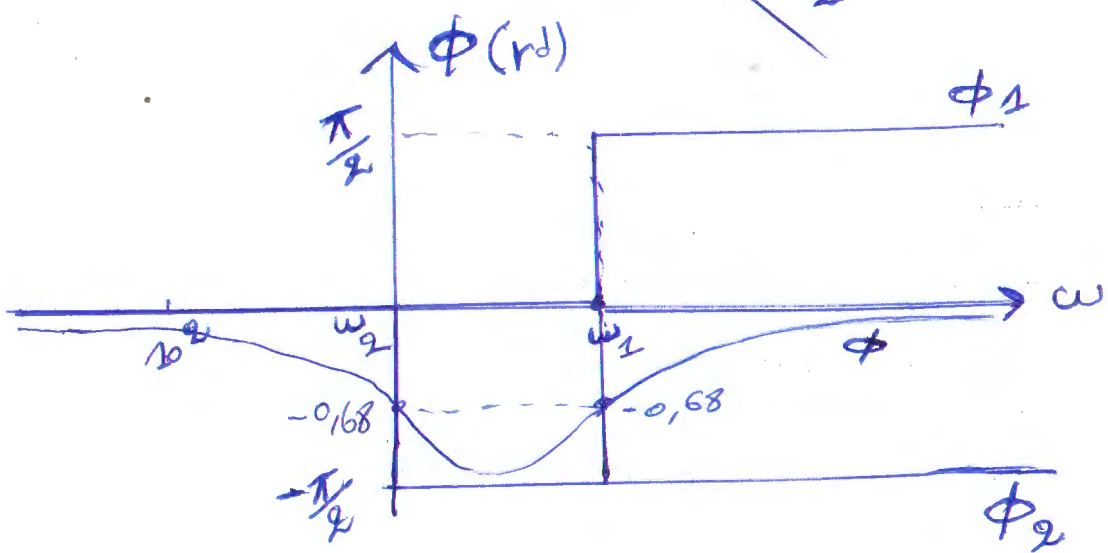
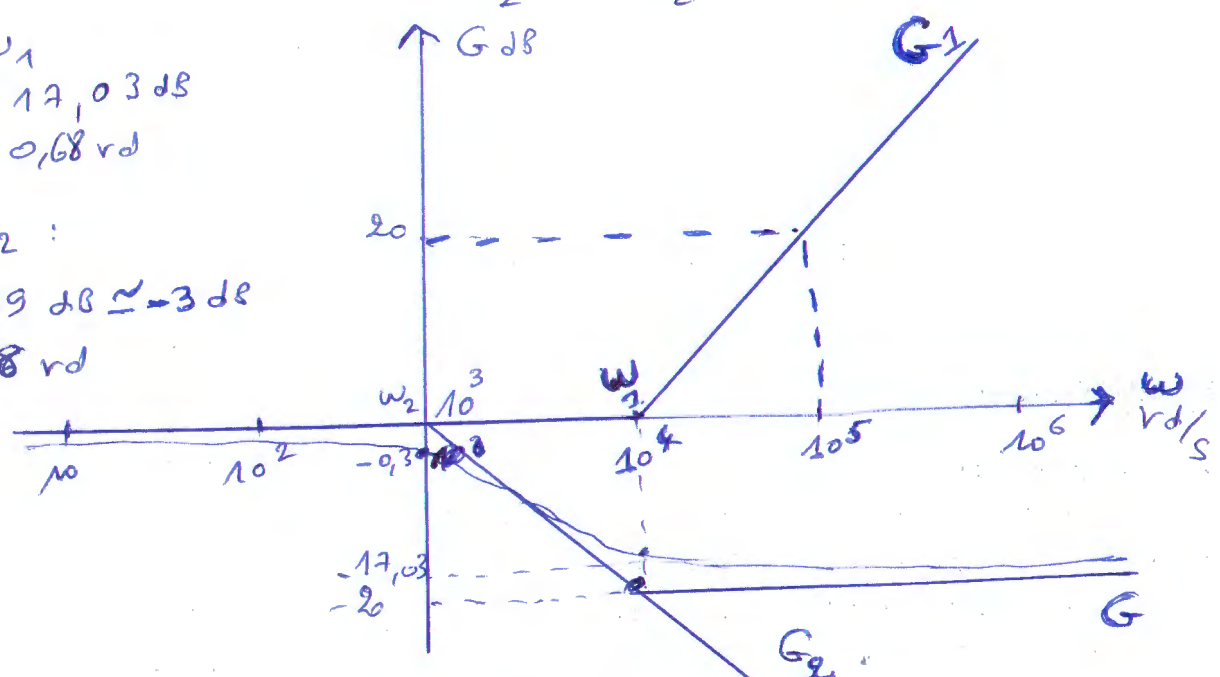
Les asymptotes :

$G_1, \phi_1$  :  $\omega \ll \omega_1$   $\left\{ \begin{array}{l} G_1 = 0 \text{ dB} \\ \phi_1 = 0 \text{ rd} \end{array} \right.$   
 $\omega \gg \omega_1$   $\left\{ \begin{array}{l} G_1 = 20 \log \frac{\omega}{\omega_1} \rightarrow \text{droite de pente } 20 \text{ dB/décade} \\ \phi_1 = \frac{\pi}{2} \text{ rd} \end{array} \right.$

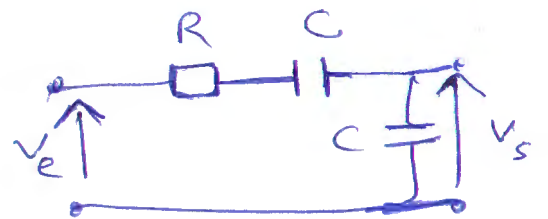
$G_2, \phi_2$  :  $\omega \ll \omega_2$   $\left\{ \begin{array}{l} G_2 = 0 \text{ dB} \\ \phi_2 = 0 \text{ rd} \end{array} \right.$   
 $\omega \gg \omega_2$  :  $\left\{ \begin{array}{l} G_2 = -20 \log \frac{\omega}{\omega_2} \rightarrow \text{droite de pente } -20 \text{ dB/décade} \\ \phi_2 = -\frac{\pi}{2} \text{ rd} \end{array} \right.$

pour  $\omega = \omega_1$   
 $\left\{ \begin{array}{l} G = -17,03 \text{ dB} \\ \phi = +0,68 \text{ rd} \end{array} \right.$

pour  $\omega = \omega_2$  :  
 $\left\{ \begin{array}{l} G = -2,99 \text{ dB} \approx -3 \text{ dB} \\ \phi = -0,68 \text{ rd} \end{array} \right.$



Exercice N° 11 :



on utilise le diviseur de tension pour calculer la fonction de transfert :

$$H(j\omega) = \frac{V_S}{V_e} = \frac{\frac{1}{j\omega C}}{R + \frac{1}{j\omega C} + \frac{1}{j\omega C}} = \frac{1}{j\omega C} \times \frac{j\omega C}{2 + jRC\omega}$$

$$= \frac{1}{2 + jRC\omega} = \frac{1}{2} \cdot \frac{1}{1 + j\frac{RC\omega}{2}} = K \frac{1}{1 + j\frac{\omega}{\omega_0}}$$

avec :  $K = \frac{1}{2}$  ;  $\omega_0 = \frac{2}{RC}$  rd/s = 10 rd/s.

\* Le gain en dB :

$$G_{dB} = 20 \log_{10} K - 20 \log_{10} \sqrt{1 + \left(\frac{\omega}{\omega_0}\right)^2} = G_1 + G_2$$

\* La phase :  $\phi = 0 - \arctg \frac{\omega}{\omega_0} = \phi_1 + \phi_2$

Les asymptotes :

$$G_2, \phi_2 : \omega \ll \omega_0 \begin{cases} G_2 = 0 \text{ dB} \\ \phi_2 = 0 \text{ rd} \end{cases}$$

$$\omega \gg \omega_0 : \begin{cases} G_2 = -20 \log_{10} \frac{\omega}{\omega_0} \rightarrow \text{droite de pente } -20 \text{ dB/décade} \\ \phi_2 = -\frac{\pi}{2} \text{ rd} \end{cases}$$

